

CITY OF WEST KELOWNA DEVELOPMENT PERMIT WITH VARIANCES DP 23-14

To: Jenifer Berkhiem 105-1932 Summit Drive Kelowna, BC V1V 3E9

- This Development Permit is issued subject to compliance with all the Bylaws of the City of West Kelowna applicable thereto, except as specifically varied or supplemented by this Permit.
- 2. This Permit applies to and only to those lands within the City of West Kelowna described below, and any and all buildings, structures, and other developments thereon:

PLAN EPP67384 LOT 14 DISTRICT LOT 3496 OSOYOOS DIV OF YALE DISTRICT (3053 Wales Rd)

- 1. This Permit Hillside Development Permit with Variances allows for the development of a Single family dwelling in a Hillside Development Area with the following variances S.10.5.5(g)i. of the Zoning Bylaw to reduce the front parcel boundary setback from 6.0 m to 0.9 m for the garage and 4.5m to 3.0 m and S.10.5.5(f)i. of the Zoning Bylaw to increase the building height from 10.0 m to 11.32 m. subject to the following conditions and related Schedules:
 - A. The size and dimensions of the single family dwelling are to be in accordance with Schedule 'A':
 - B. The dimensions, siting, and parking layout are to be in accordance with Schedule 'B';
 - C. The landscape works to be in accordance with Schedule 'C';
 - D. Landscape Estimate works to be in accordance with Schedule 'D';
 - E. All construction activities to be conducted on the land in general accordance with Schedule 'E'.
- 2. As a condition of the issuance of this Permit, the City of West Kelowna is holding a landscape security set out below to ensure that development is carried out in accordance with the terms and conditions of this Permit. Should any interest be earned upon the security, it shall accrue to the Permittee and be paid to the Permittee if the security is returned. The condition of the posting of the security is that should the Permittee fail to carry out the development hereby authorized, according to the terms and conditions of the Permit within the time provided, the City of West Kelowna may use the security to carry

out the work by its servants, agents or contractors, and any surplus shall be paid over to the Permittee, or should the Permittee carry out the development permitted by this Permit within the time set out below, the security shall be returned to the Permittee. There is filed accordingly:

An Irrevocable Letter of Credit or Bank Draft in the amount of \$23,125.00

- 3. The land described herein shall be developed strictly in accordance with the terms and conditions of this Permit and any plans and specifications attached to this Permit, which shall form a part hereof. Should any change be required to this permit, please ensure that you obtain written approval from the City of West Kelowna prior to making any changes.
- 4. If this Development Permit has not been issued within one year from approval, Permit (DP 23-14) shall be deemed to have been refused and the file will be closed.
- 5. This Permit is not a Building Permit.
- 6. This Permit is not a Municipal Highway Permit.
- 7. This is not an Archaeology Permit.

A: All archaeological sites in B.C. are protected under the Heritage Conservation Act. This applies to whether sites are located on public or private land and whether the site is known or unknown. If you think you have uncovered an archaeological site during a building project or renovation, please do not disturb the site further and call B.C.'s Archaeology Branch immediately at (250) 953-3334. Branch archaeologists will review your project plans and make recommendations to manage site impacts and secure the required permitting.

AUTHORIZING RESOLUTION NO (XXXXXXXX) PASSED BY THE MUNICIPAL COUNCIL ON (DATE).

	Signed on
	Corporate Officer
I hereby confirm that I have read and concur with the ensure that copies of the Permit will be provided to on	
	Signed on
	Property Owner or Agent
ISSUED on	
Schedules:	

Schedule A: Architectural Plans prepared by R-Tistry Home Design on August 31st, 2023.

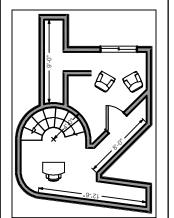
Schedule B: Site Plan prepared by Vector Geomatics Land Surveying Ltd. on January 5th, 2023.

Schedule C: Landscape Plan prepared by Shelley Lynn Design on September 5th, 2023.

Schedule D: Landscape Estimate prepared by Picture Perfect Landscaping on September 11th, 2023.

Schedule E: Slope Stability Report prepared by Evertek Engineering Ltd. on August 31st, 2023.





R-tistry Home Design.com

NO.3 FOUNDATION/ CRAWL SPACE REV. AUG. 8-2023
NO.4 BUILDING HEIGHT VARIANCE AUG. 9-2023
NO.5 PROJECT SUMMARY UPDATE AUG. 31-2023

3053 WALES RD.
WEST KELOWNA, BC

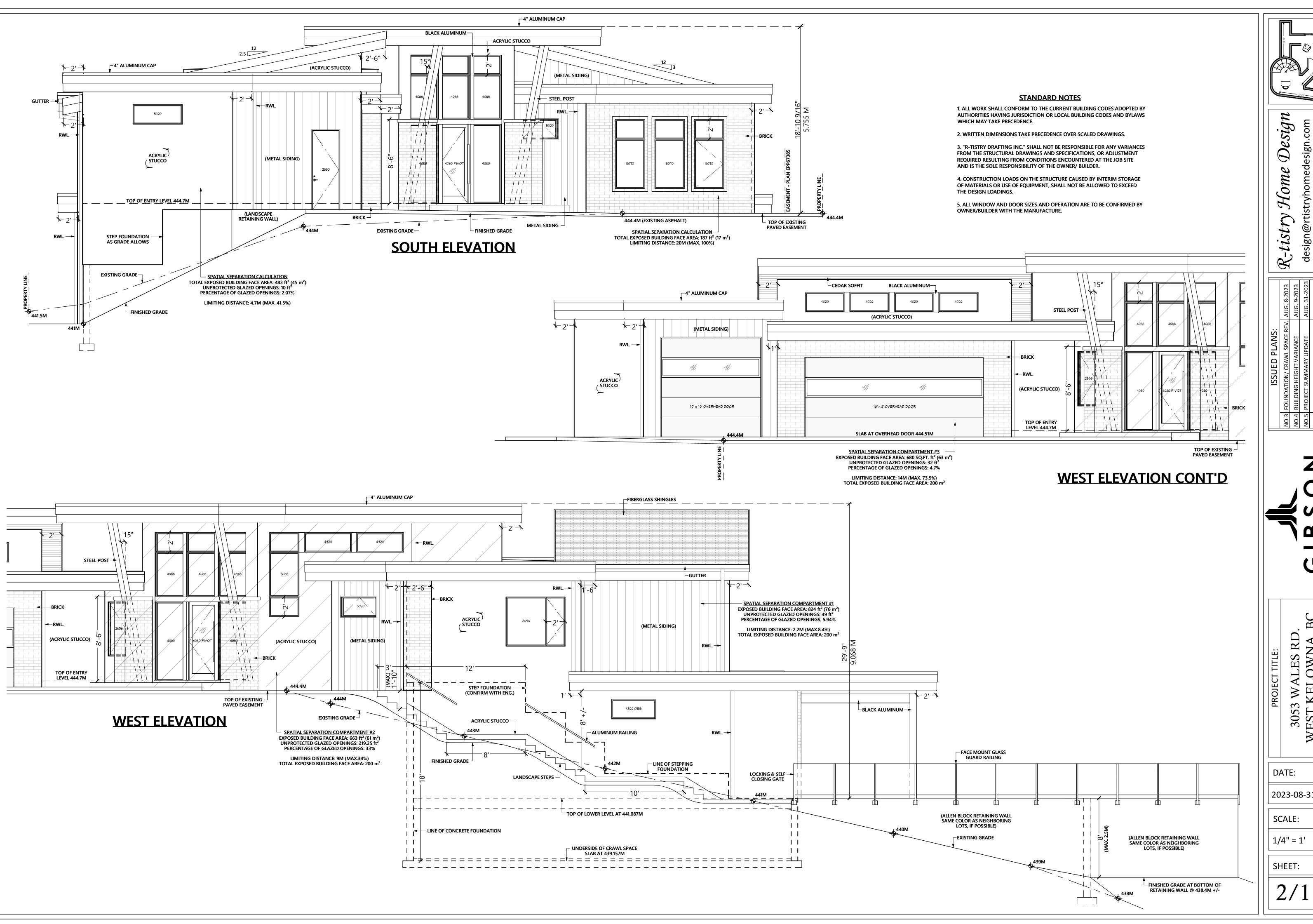
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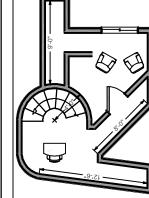
2023-08-31

SCALE:

1/4" = 1'

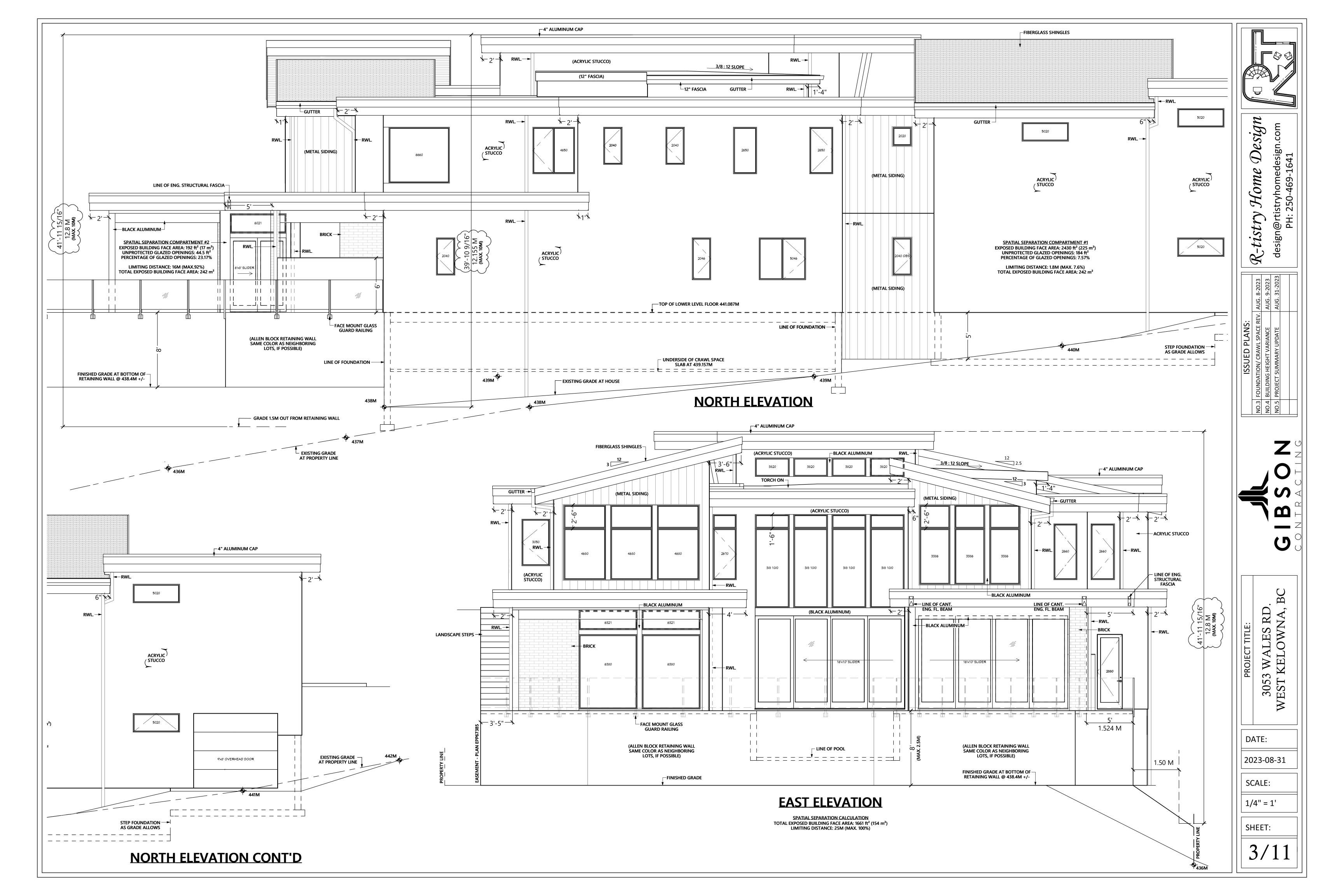
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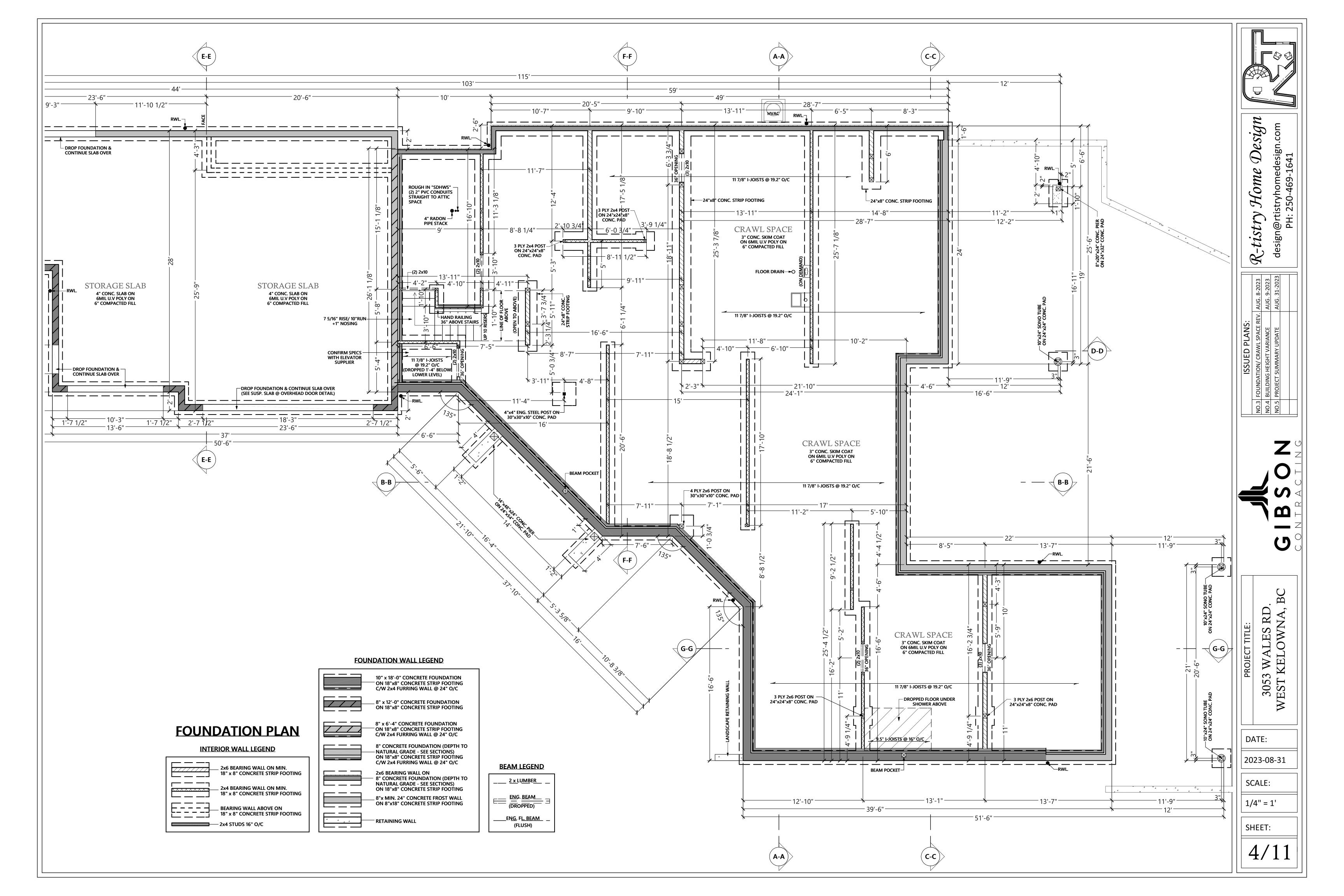


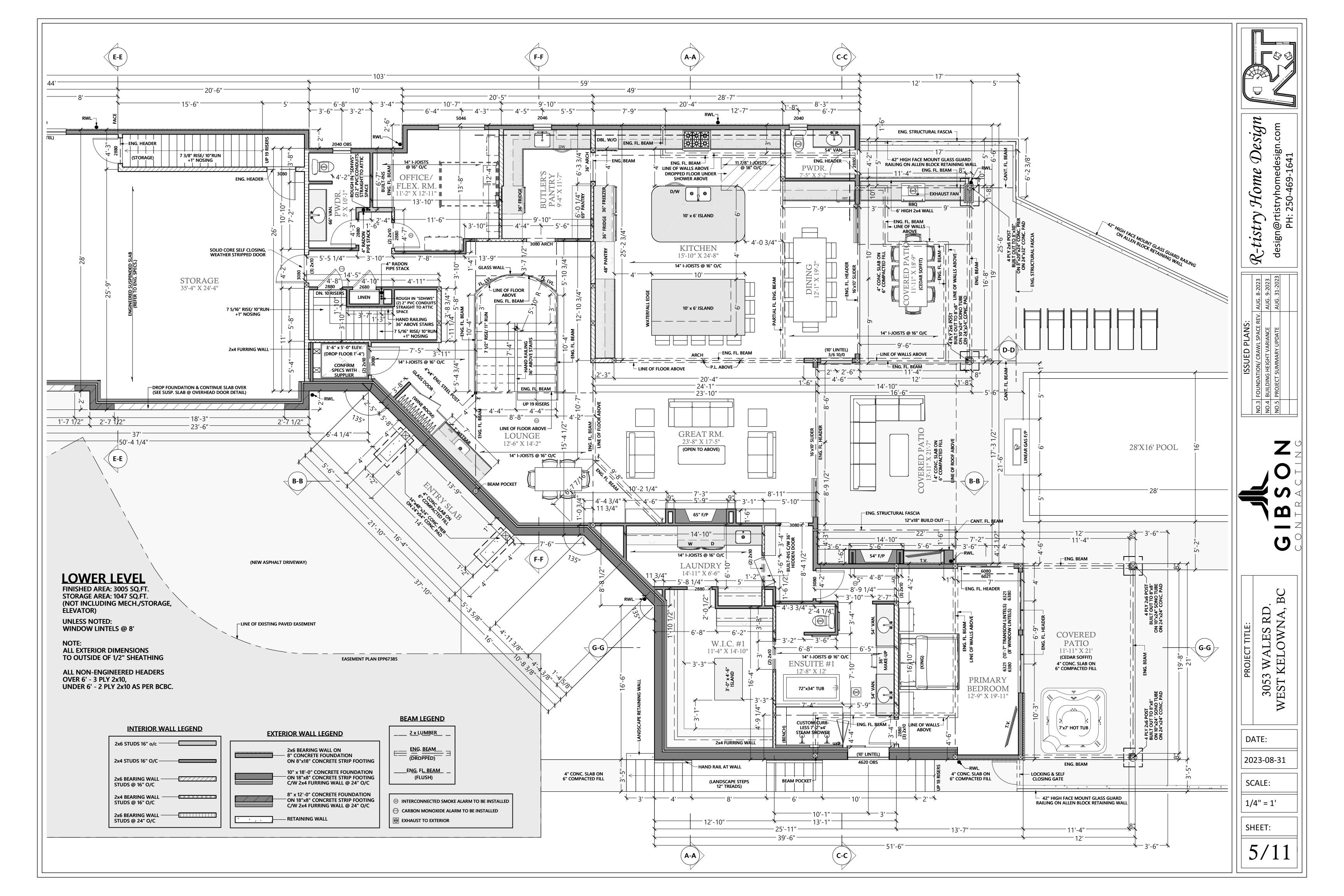


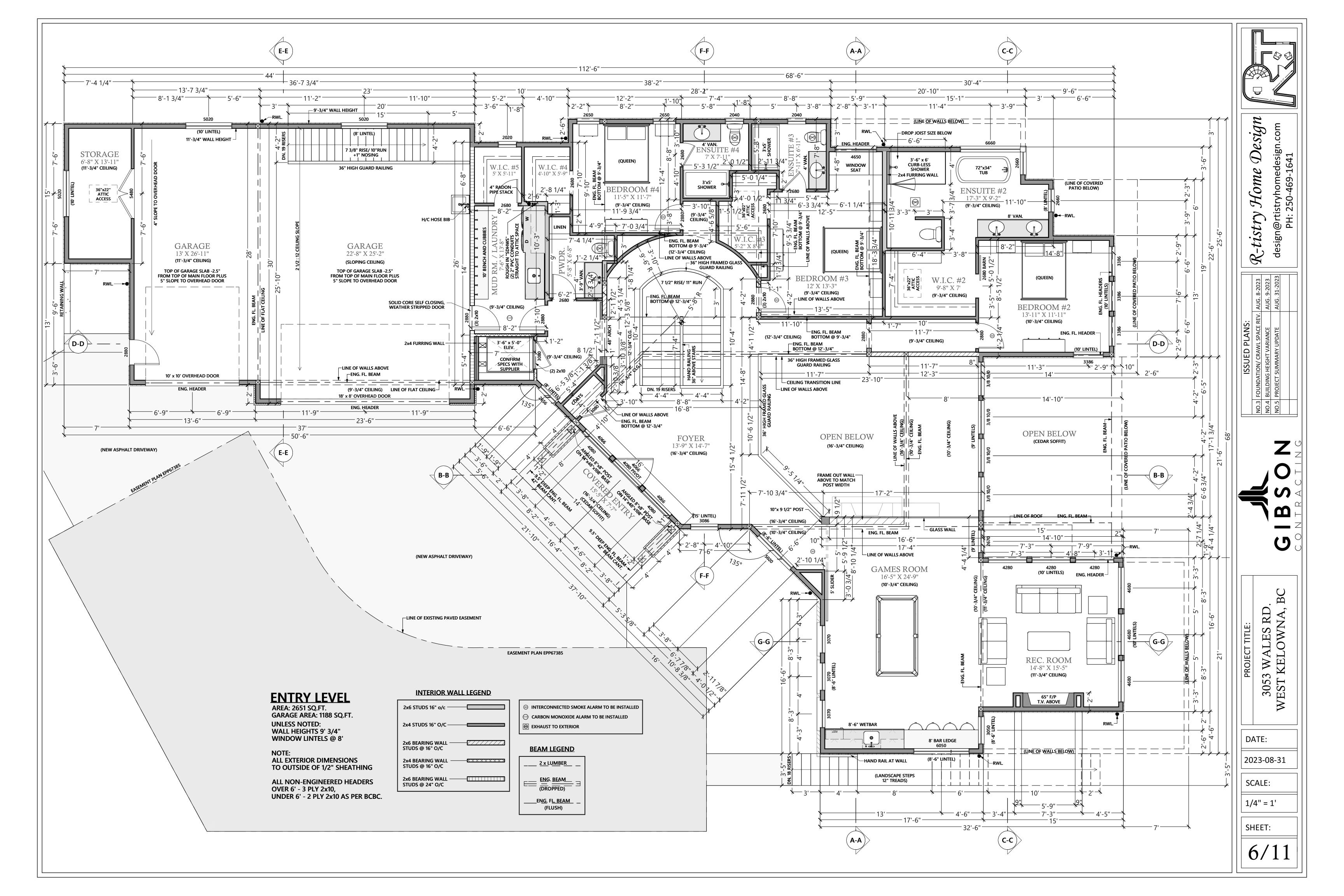
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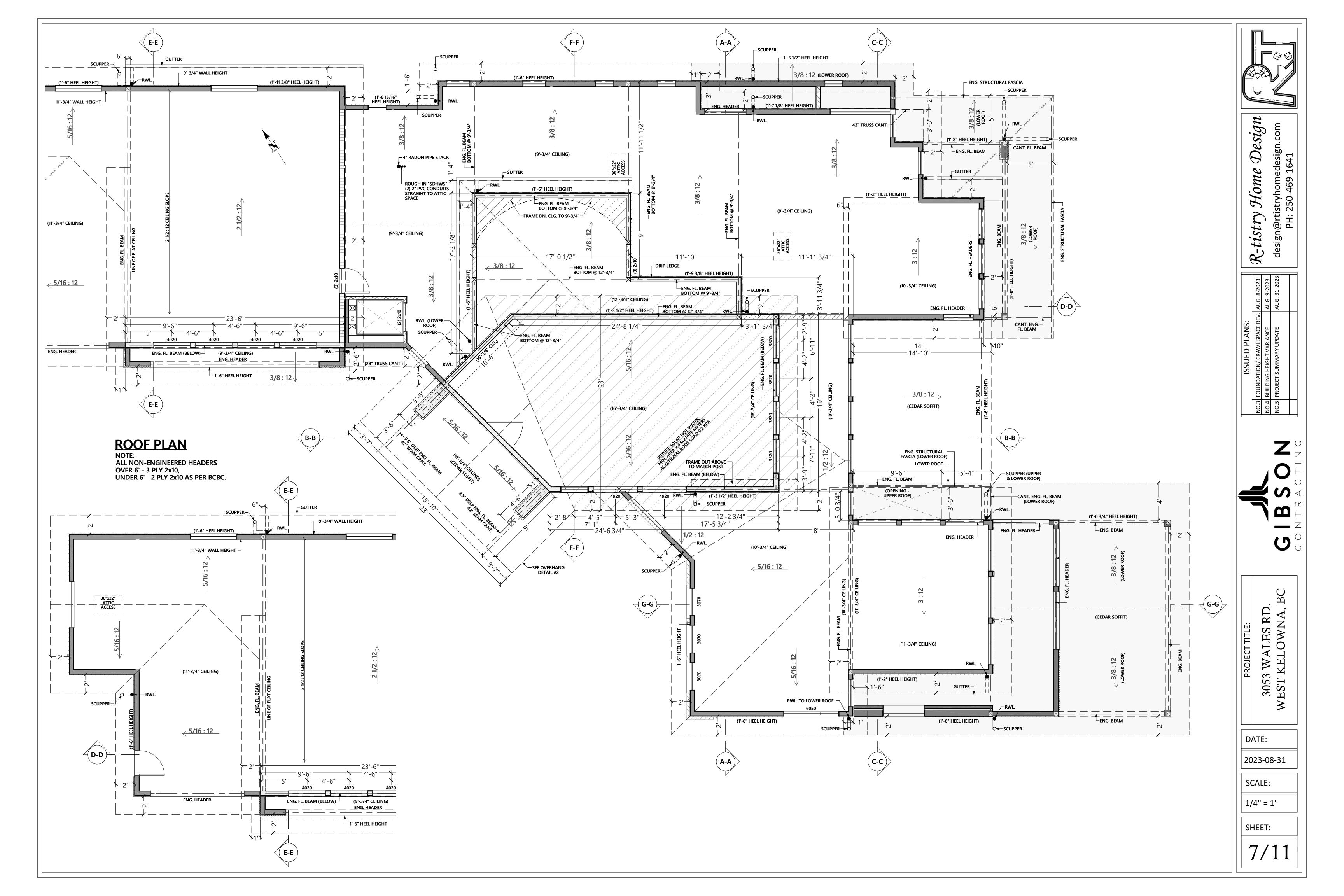
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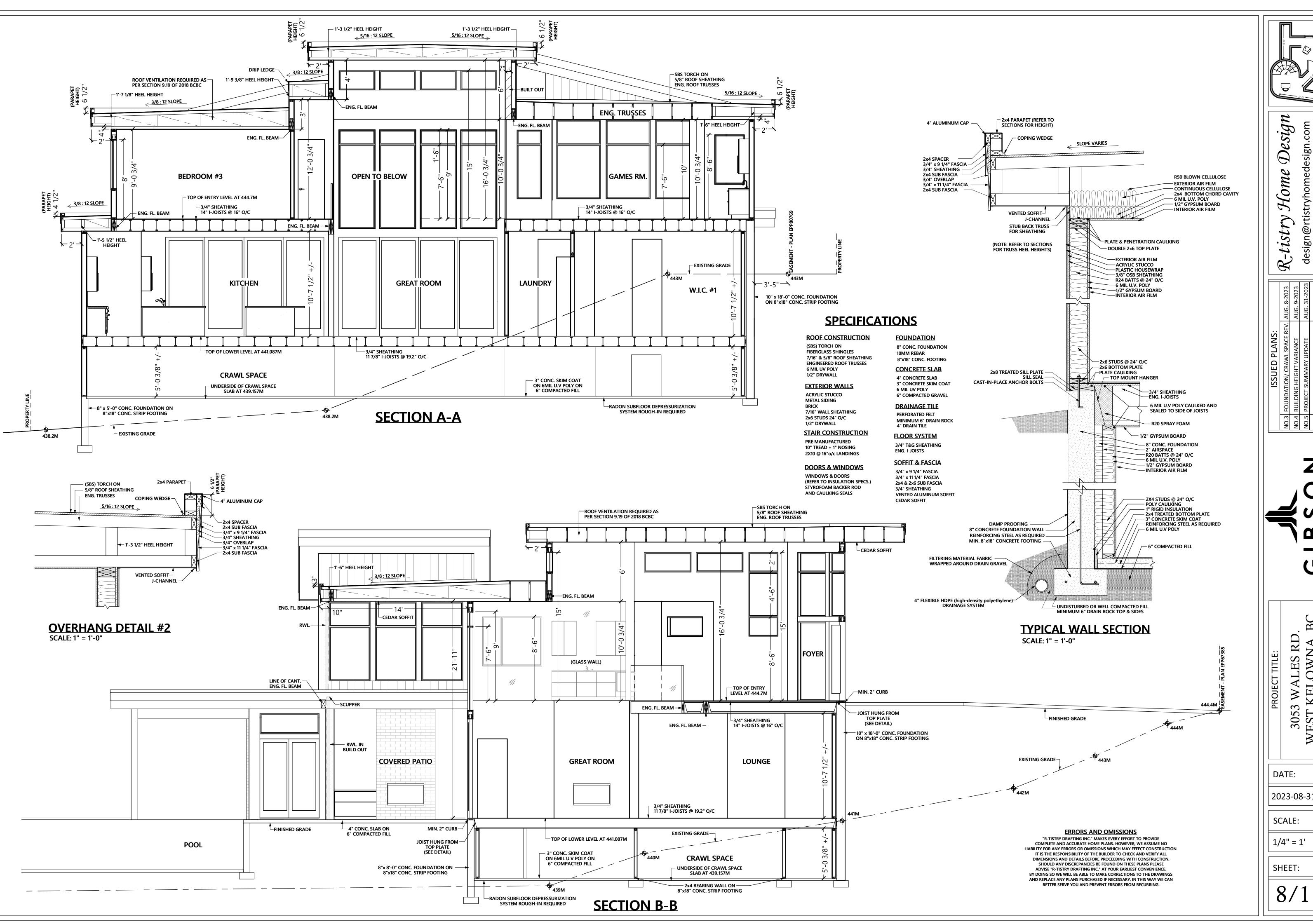










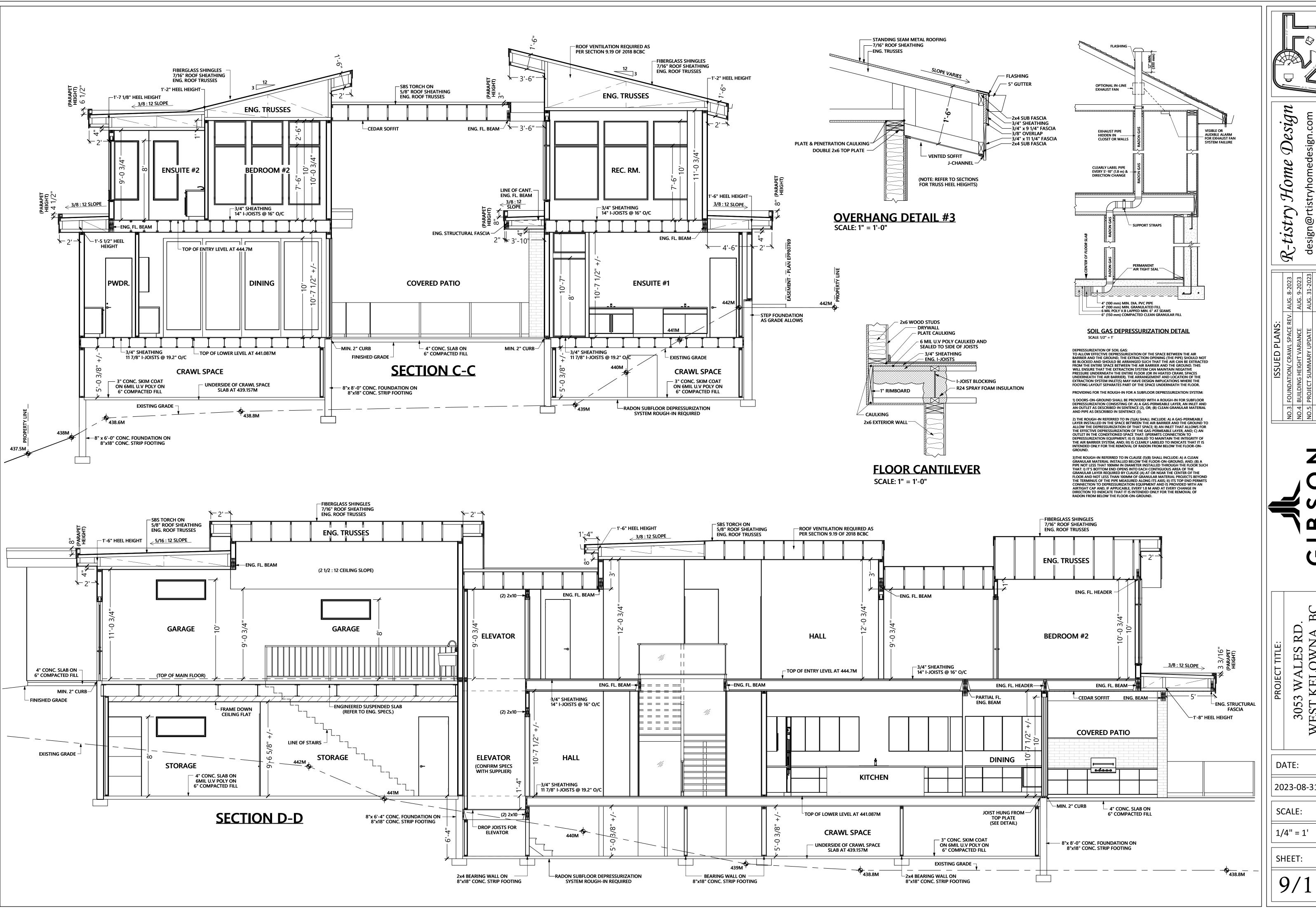


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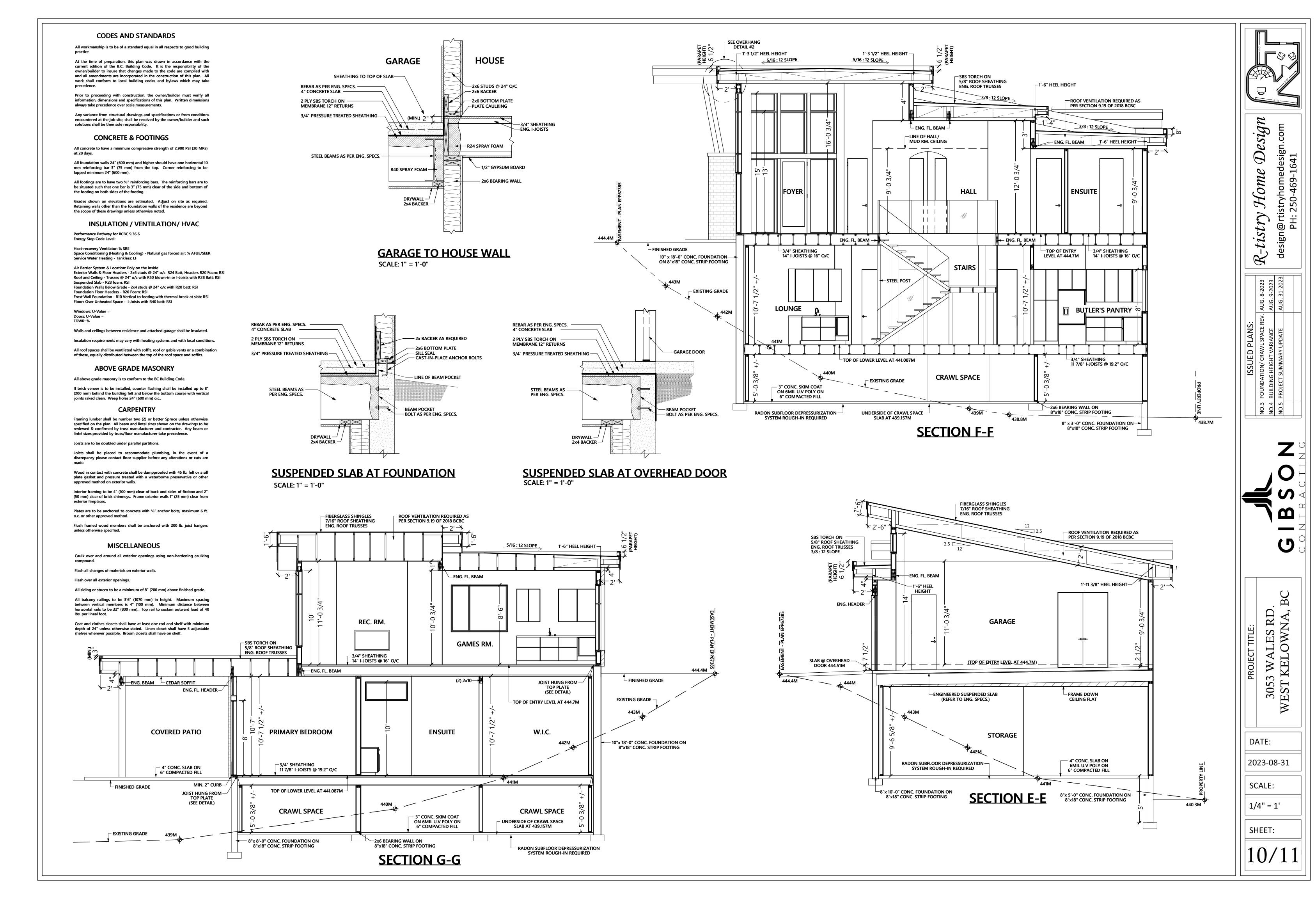


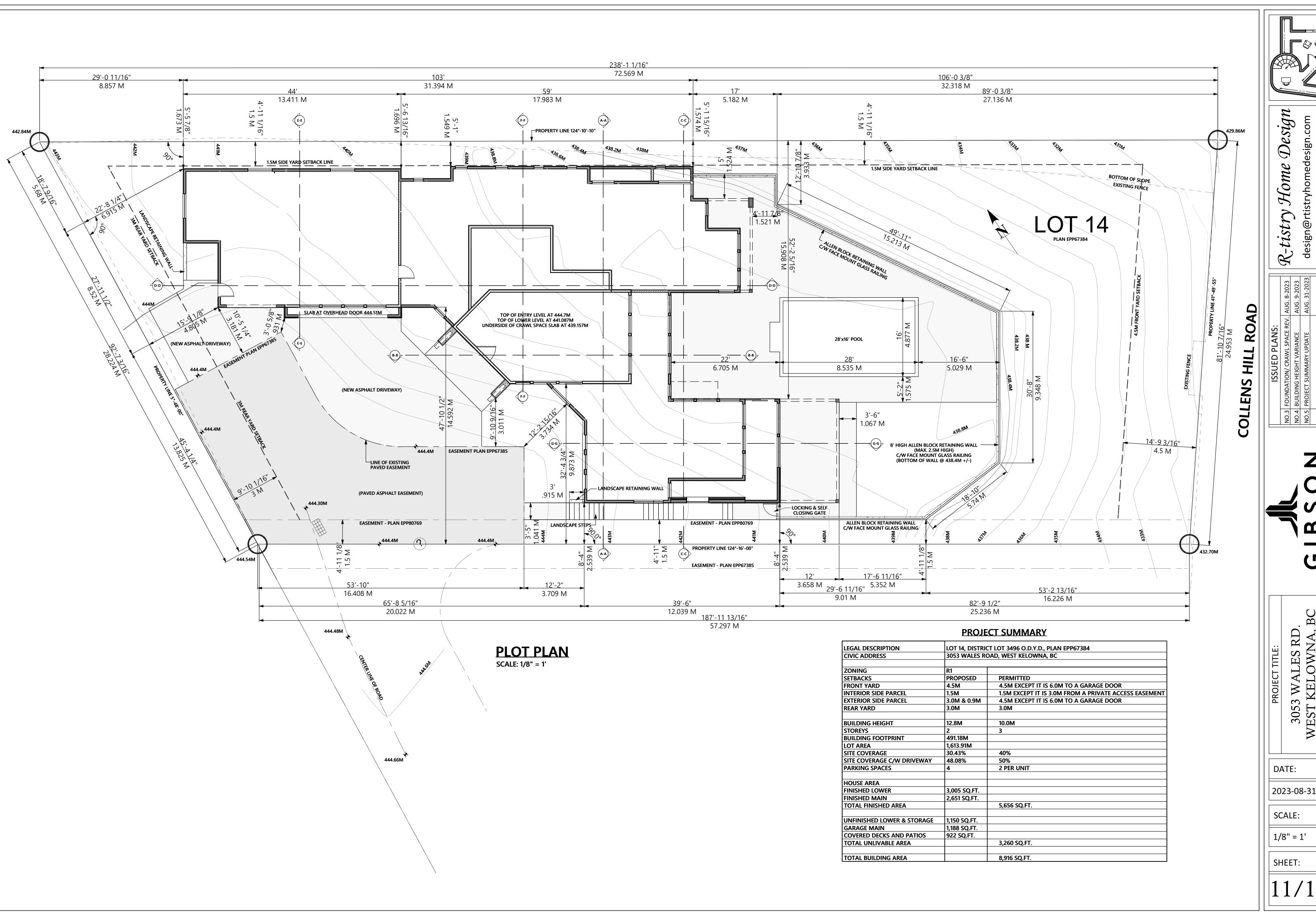
| ISSUED PLANS:
| FOUNDATION/ CRAWL SPACE REV. | AUG. 8-3

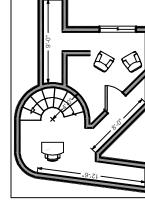
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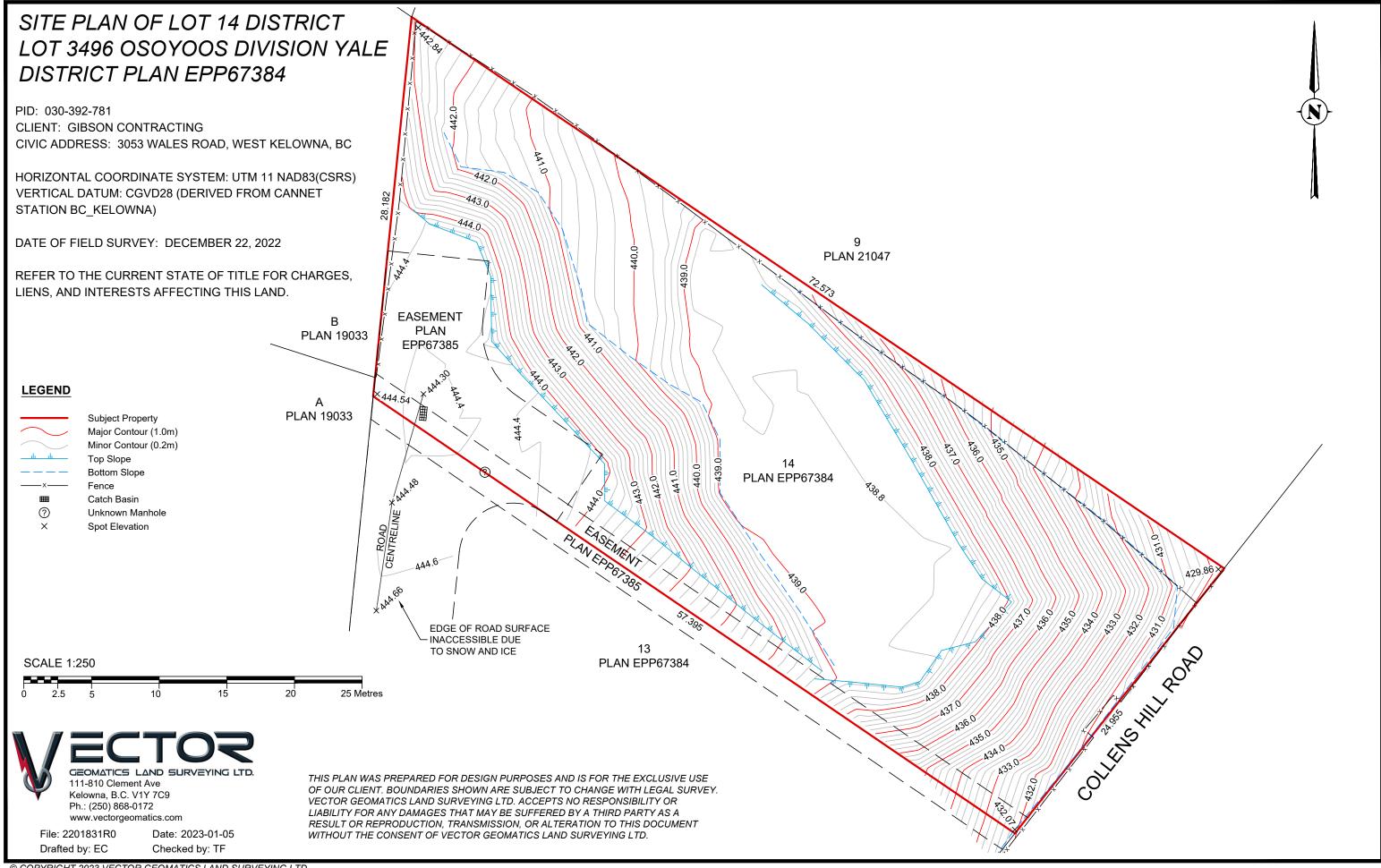




3053 WALES RD. VEST KELOWNA, I

2023-08-31

SHEET:





shelleylynndesign@gmail.com

ORTYNSKI, Jessa & Cory 3053 Wales Road			
lent:	West Kelowna, BC		
cde	date	revision	
1:18	September 5, 2023	REV002	
rawn by	checked by	drawing #	
S.WEMPE	J.BERK	3053WAL	

PRELIMMARY DESIGN ONLY.
THE GUANTITIES SHOWN ON THE LABELS ARE NOT TO BE CONSTRUED AS THE COMPLETE AND ACCURATE LIMITS
OF THE CONTRACT.

WARRANTIES ARE NULL AND VOID DUE TO DAMAGE FROM WILDLIFE SUCH AS DEER, RABBITS, VOLES AND OTHER RODENTS. ALTHOUGH PLANTS LISTED MAY BE RATED AS RESISTANT TO THESE ANMAL SPECIES, IT IS NOT GUARANTEED ACCURATE.

CLIENT'S SIGNATURE OF ACCEPTANCE
THIS SIGNATURE AUTHORIZES THE CONTRACTOR TO PROCEED WITH THE CONSTRUCTION OF THIS PROJECT
AS PRESENTED BY THIS DESIGN

This signature also acknowledges the scope and details of the project as represented by this design. Any subsequent changes must be made via change order and will result in additional costs.

DEVELOPER'S SIGNATURE OF ACCEPTANCE

LANDSCAPE NOTES:

ALL PLANT BEDS TO BE 2" COBBLE ROCK MULCH EXCEPT WHERE OTHERWISE INDICATED

ALL MEASUREMENTS AND QUANTITIES TO BE CONFIRMED ALL LANDSCAPING TO FOLLOW BCLNA GUIDELINES

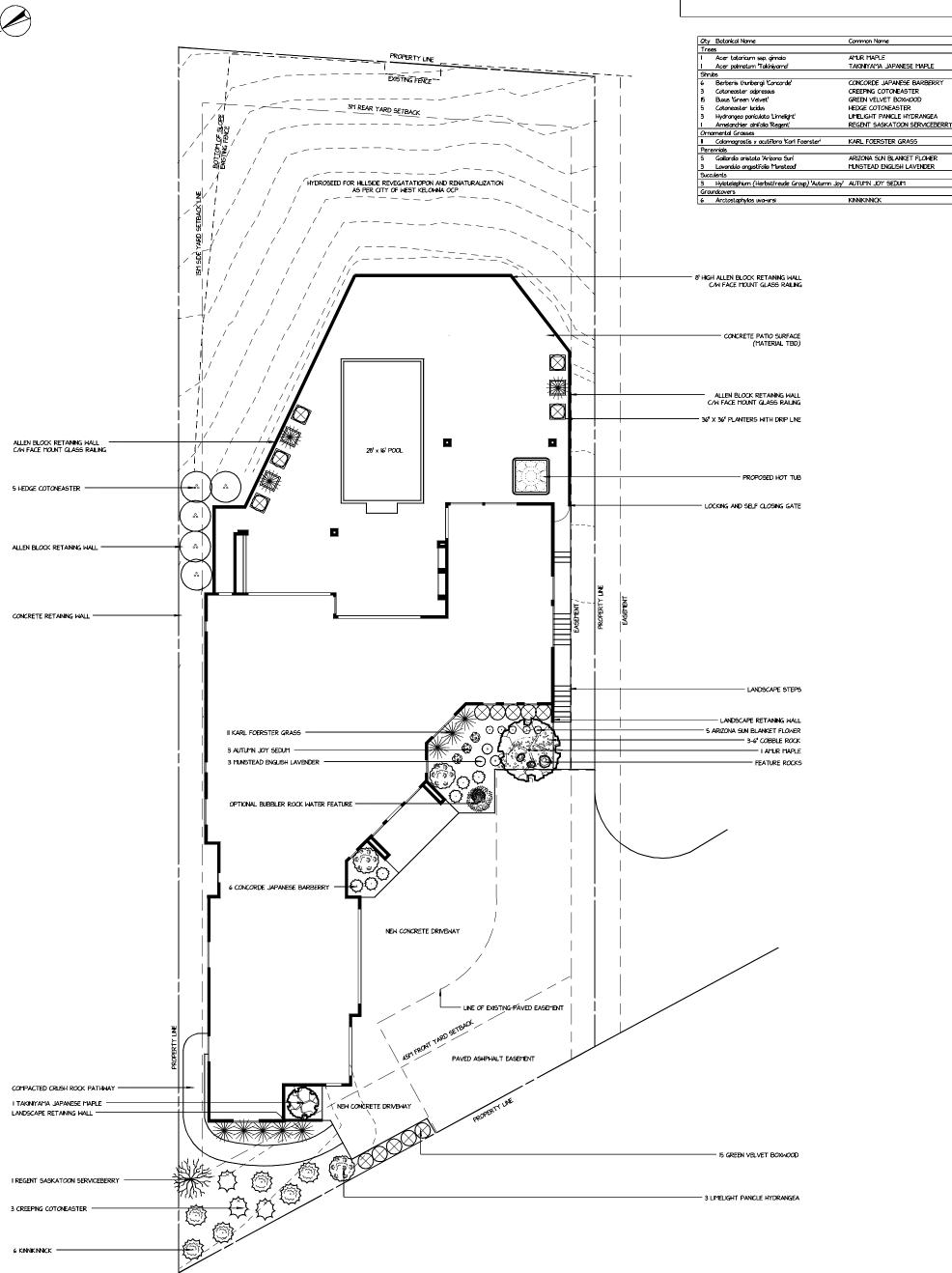
ALL IRRIGATION TO BE DRIP LINE FOR PLANTS WITH TIMED CONTROLLER AS PER BCLINA GUDELINES

ALL LANDSCAPING TO MEET FIRESMART REGULATIONS BACK SLOPE TO BE HYDROSEEDED AS PER CITY OF WEST KELOWNA OCP

TREES TO BE 10-15 GAL POT SIZE ALL SHRUBS TO BE MIN 2 GAL POT SIZE ALL PERENNALS AND ORNAMENTAL GRASSES TO BE MIN I GAL POT SIZE

PLANT DISCLAIMER

DUE TO COVID-19 CIRCUMSTANCES AFFECTING THE NURSERY INVENTORES, PLANT SUBSTITUTIONS MAY BE NECESSARY, IN THE EVENT THAT A PLANT LISTED ABOVE CANNOT BE OBTANED, A CLOSE AND SIMILAR PLANT SPECIES MAY BE INSTALLED IN 11'S PLACE.



Picture Perfect Landscaping

11131 Pheasant Rd. Winfield, British Columbia V4V 1W9

QUOTE

Quote No.: 298

Date: 09/11/2023

Page: Ship Date:

Sold To: Ship To:

Gibson Contracting Gibson Contracting

Kelowna, BC Kelowna, BC

Business No.: 846694156RT0001

Ougntity		840094150R10001	Unit Prins	Tev	Amount
Quantity	Unit	Estimate for Landscaping at 3053 Wales Rd, Westside, as per plan provided to us. Measurements showing landscaping only to front property line and need to be verified on site Rear landscaping on left side to back of Cotoneaster plantings only, and on right side to gate shown. Approx 1800 s/f xeriscaped garden areas to be planted as shown, complete with weed barrier fabric and topped with 1" crushed silver granite unless otherwise shown. Crusher chip pathway to be done in weed barrier fabric and black crusher chips 1" crushed silver granite down both sides of house with weed barrier fabric installed Extra drip lines run to rear deck pots All plants and trees on automatic drip irrigation Conduit to be installed under any hardscaping as needed to planted areas Roughed in irrigation and power to be installed by builder to outside area reasonable for propririgation services to be installed Includes supplies, labour, materials, delivery and \$2250 plant budget All prices subject to GST Any onsite changes will incur cost adjustments as needed Although some plants may be rated as deer resistant, it cannot be guaranteed and warranties will not cover damage from wildlife. Plants may be substituted for like kind depending on availability at time of install 25% Deposit required for materials before any project begins	as r er	Tax	Amount 18,500.00
Shipped by Comments Sold By:	30 d	ay estimate subject to change due to product availibility, and any unforseen excavation s.	Total Amount		18,500.00



Our File: E100864

August 31, 2023

Gibson Contracting 105-1932 Summit Drive Kelowna, BC V1V 3E9

Attn: Ms. Jenifer Berkhiem

Email: jenifer@gibsoncustomhomes.com

Re: Slope Stability Assessment for the Proposed Single-Family Dwelling

3053 Wales Road, West Kelowna, BC

1.0 Introduction

Evertek Engineering Ltd. (Evertek) was retained by Gibson Contracting (the Client) to prepare this slope stability assessment report for the proposed single-family dwelling on the property located at 3053 Wales Road in West Kelowna, BC. According to the City of West Kelowna Official Community Plan (OCP) Bylaw 100.42, the site is within the Hillside Development Permit Area (DPA 4) with steep slopes. Therefore, a development permit (DP) with a site-specific geotechnical hazard (steep-slope) assessment is required for the proposed building. This report has been prepared based on Evertek's scope of work outlined in our Confirmation of Assignment dated July 25, 2023. This report does not address environmental considerations.

The purposes of this slope stability assessment were:

- To conduct a field review of the current site surface and subsurface conditions;
- To review surficial geology in the area;
- To identify potential geohazards on the site, and to provide geotechnical recommendations for mitigation of the geohazards and protection of the natural environment; and
- To comment on the suitability of the site for the proposed residential development.

Preparation of this report is generally in accordance with the following guidelines and bylaws:

- West Kelowna Official Community Plan Bylaw 2011 No 0100;
- British Columbia Building Code 2018; and
- Professional Practice Guidelines Landslide Assessments in British Columbia. Version
 4.1. Engineers and Geoscientists British Columbia. Revised March 2023.

This report has been prepared using the information provided by the Client and the topographic survey plan prepared by Vector Geomatics Land Surveying Ltd. (Dated: January 1, 2023). The Geotechnical Investigation Report for the Proposed 14 Lot Single-Family Development at 3055 Thacker Drive, West Kelowna, BC prepared by Beacon Geotechnical Ltd. (dated: June 8, 2016, revised July 25, 2017) was reviewed when preparing this report.



2.0 Site Location & Proposed Development

The property is identified with the civic address and legal lot description as 3053 Wales Road, West Kelowna, BC – Lot 14, Plan EPP67384, District Lot 3496, Osoyoos Division of Yale Land District, PID: 030-392-781. The site location is shown in the attached Figure 1. The total area of the property is 0.398 acres (1,610 m²).

The property is currently sloping down to the east with localized steep slopes with an inclination of approximately 28 to 32 degrees. Based on the architectural plan prepared by R-tistry Home Design (dated: July 10, 2023), it is understood the Client is planning to construct a 2-storey residential single-family building with a crawl space on the property. An Allan block retaining wall is being proposed in the backyard above the natural slope to raise the backyard in order to have a pool at the walkout (lower level) house elevation.

3.0 Background Information

3.1 Surficial Geology

Based on the published information from the Geological Survey of Canada (Kelowna, Surficial Geology Map 6146), the surficial geology of the subject site is expected to be underlain by Glacial Sediments, continuous till cover (Tb): Diamicton comprising lodgement and ablation facies with thicknesses generally over 1 m. The diamicton consists of a heterogeneous mixture of boulder, cobbles, pebble, sand, silt and clay. In the Kelowna area, granitic rocks tend to produce a more gravelly sandy till compared to Tertiary bedrock resulting in a more clay-rich till.

3.2 Seismic Design Data

Based on published information from Natural Resources Canada, for site Class D (stiff soil) as per 2020 National Building Code Seismic Hazard, a seismic event with a 2% probability of exceedance in 50 years at the project site would have peak ground acceleration (PGA) of 0.113g (9.81m/s²). The spectral acceleration for Class D is presented in Table 1.

Table 1: Spectral accelerations (g) for Class D for return period of 2475 years

- 1				,			
	Sa(0.2)	Sa(0.5)	Sa(1.0)	Sa(2.0)	Sa(5.0)	Sa(10.0)	PGA
	0.271	0.261	0.202	0.143	0.0663	0.0327	0.113

4.0 Field Geotechnical Investigation

A field subsurface investigation was conducted on August 11, 2023. A total of two (2) test pits (TP23-01 to TP23-02) were excavated to depths ranging from approximately 1.5 m to 2.4 m below the existing grade. The approximate test pit locations are shown in Figure 2, attached. The test pits were backfilled with the excavated soils and nominally compacted with the bucket of the excavator. It should be noted that the test pits indicate subsurface conditions encountered at the respective test pit locations only. The subsurface conditions may vary outside the test pit locations and below the depth explored.

Test pit TP23-01 encountered Fill to the test pit termination depth of 2.4 m below the existing grade. The Fill consisted of dry to damp, compact to dense angular blast rock fragments mixed with silty sand and occasional rootlets. The consistency at the bottom of the test pit TP23-01 was



very dense. Test pit TP23-02 encountered a 1.05 m thick surficial layer of Fill (damp, compact angular blast rock fragment mixed with silty sand and occasional rootlets) underlined by damp, compact to dense silty sand. Test pit T23-02 was terminated in the native silty sand layer at a depth of 1.5 m below the existing grade due to mechanical refusal. No groundwater was encountered at all test pit locations. A detailed description of subsurface conditions encountered in the test pits is provided in test pit logs, attached. Based on the geotechnical report by Beacon Geotechnical, during their field work, the borehole BH-08, near the subject lot, encountered refusal at 2 m below the existing grade due to cobbles or boulders which could indicate bedrock in the near vicinity.

Site surface conditions including surficial soil, slopes, and surface drainage were visually examined. Field observations are summarized below:

- The property is currently vacant and covered with some grass and shrubs.
- An existing common paved laneway easement with a hammerhead turnaround is located at the west corner of the property.
- A building pad was established which was relatively flat. There were localized steep slopes above the building pad towards the laneway easement to the west and below the building pad towards Collens Hill Road (east).
- The localized steep slopes have a measured inclination of approximately 28 to 33 degrees. The elevation difference in the proposed building area is approximately 20 ft (6.0 m) while the ground surface relief for the entire property is approximately 47.5 ft (14.5 m) according to the topographic site plan.
- Neither surface drainage nor ponding water was noted at the time of our field review.
- Signs (tension cracks and failure scarps) of past landslides on a considerable scale were not identified at the time of our site observation.

Selected photographs showing the current site conditions are attached.

5.0 Slope Stability Assessment

Due to the hilly nature of the site, stability of site slopes is the most important factor in consideration for the proposed development. An adequate setback for the proposed building from steep slopes should be implemented during the design and construction. The near-surface sand contains fines which are prone to erosion if exposed. Erosion control must be implemented during construction. These potential geotechnical concerns will be further addressed in the following sections.

5.1 Slope Stability Analysis

To evaluate the stability of the natural slopes on-site, a global slope stability analysis was performed using commercial software, Rocscience Slide2D. The global slope stability was analyzed using the limit equilibrium method. Two cross sections were selected for the analysis. Cross Section A-A had the most critical slope (32°), and Cross Section B-B was selected in an area where the proposed house is close to the steep slope (approximately 3 m away). The site plan showing the location of the cross sections used for the slope stability analysis is shown in Figure 3, attached. Based on the geotechnical report by Beacon Geotechnical, the recommendation of 3 m setback from house foundation to fill slopes is recommended.



The soil profile for the analysis was based on the results of our field visual observation of the slope and subsurface information collected from the test pits during the field geotechnical investigation.

The Janbu limit equilibrium analysis method was used to analyze the slope. The circular failure mechanism with multiple failure surfaces was assumed.

Soil parameters were estimated based on our field observations and general experience with local soils of a similar type and state. Soil parameters, used in the slope stability analysis, are summarized in Table 2 below.

Table 2. Assumed soil parameters

Soil Type	Unit Weight, kN/m³	Cohesion, kPa	Friction angle, degrees
Fill (Blast rock fragment mixed with silty sand)	20	0	40
Silty Sand	19	5	37.5

To account for earthquake loading, pseudo-static seismic analysis was conducted together with a static case. The Peak Ground Acceleration (PGA) for this site is 0.113g for a probability of occurrence of 2% in 50 years, which was obtained from the website of National Resources Canada as listed above. In seismic slope stability analysis, the seismic force was introduced as a constant lateral force applied to the centre of gravity of the potential sliding mass.

The results of the analysis are presented in Figures 4 to 7, attached. The safety factors obtained from the analysis are summarized in Table 3 below.

Table 3. Slope stability analysis results

Analysis Case	Criteria Safety Factor	Calculated Minimum Safety Factor
Circular failure, Static conditions, Cross Section A-A	1.5	1.53
Circular failure, Seismic conditions, Cross Section A-A	1.0	1.22
Circular failure, Static conditions, Cross Section B-B	1.5	1.54
Circular failure, Seismic conditions, Cross Section B-B	1.0	1.24

Slope stability analysis is based upon the available soil information from the test pits. If unexpected soil conditions are encountered at the time of site development, further analysis may be required to revise the susceptibility of slope areas to undergo deformation under static and design seismic conditions.



5.2 Discussion and Recommendations

As shown in the slope stability analysis above, the safety factors (SF) against landslides under the static and seismic loading conditions are greater than the criteria SF. Therefore, the slope is considered to be stable in its current conditions. The soil in the slope predominantly comprises blast rock fill and silty sand. In the proposed building area, if loose fill and organic soil is encountered it must be removed to expose natural competent soil or blast rock fill. Granular materials such as gravel, sand and gravel, or blast rock fill may be used for restoring the site to the design grade. The structural fill to be placed in the proposed building area must be compacted adequately and reviewed by geotechnical personnel.

The sand contains fine-grained silt, which is prone to erosion. Therefore, proper measures must be implemented in the design and construction of the proposed development.

Slope Protection

Any fill slopes and disturbed natural slopes must be protected by vegetation or riprap to minimize erosion.

Site Grading and Drainage

Site grading should be designed to prevent the ponding of surface water near foundation walls, paved areas, and slope crests. Sidewalks, pavement areas, or landscaping within a zone of approximately 2 m of the exterior perimeter of the building should be graded to drain water away from the building at a minimum gradient of 2%.

Building Foundation System

Footings for the proposed building founded on the existing blast rock fill, natural silty sand, or compacted structural fill as discussed above, may be designed with a factored Ultimate Limit State (ULS) bearing pressure of 150 kPa (3000 psf) in accordance with Table 8.2 of the Canadian Foundation Engineering Manual (CFEM). The Serviceability Limit State (SLS) pressure is 100 kPa (2000 psf). The minimum width of continuous footings should not be less than 0.45 m (18 inches) and the minimum dimension of column footings should not be less than 0.90 m (36 inches).

Frost Protection

A suitable frost protection depth for the subject site is typically approximately 600 millimeters (2.0 feet).

Retaining Wall

Based on the architectural site plan, an Allan block retaining wall is proposed in the backyard, above the slope, to raise the grade to the house lower-level elevation for a pool to be installed in the backyard. The retaining wall height is 8 ft (2.4 m). Therefore, the retaining wall should be designed by a geotechnical engineer.

Liquefaction

Due to the inferred density and the nature of the observed soil conditions at the subject site, it is not expected that the natural soil deposit on site would be prone to liquefaction during a seismic event.



Further Geotechnical Recommendations

Factors of safety satisfaction only present a baseline assessment of slope conditions at the time of analysis, and may not present an accurate representation of slope conditions over the long term due to man-made processes or natural processes.

Man-made processes with the potential to negatively impact the stability of slopes and/or promote erosion include, but may not be limited to the following:

- Excavations into the slope or slope toe areas;
- Water leakage from onsite and/or offsite waterlines, storm lines, and sanitary sewer lines;
- Excessive vibration from heavy machineries, such as compaction equipment;
- Defective maintenance of slope drainage systems;
- Loading of slopes and/or slope crests (fill, structures, etc.);
- Excessive landscape watering;
- Construction of ponds, pools, or other water retention structures with potential for uncontrolled leakage;
- Removal of trees and vegetation from onsite and/or offsite areas; and

Natural processes with the potential to negatively impact the stability of the steep site slopes include, but may not be limited to the following:

- Extended periods of seasonally wet weather;
- Storm events with exceptionally high rainfall intensity and duration;
- Erosion of slope at toe areas;
- Earthquake events higher than the design event of 1:2475 events; and
- Removal of slope tree and vegetation cover by disease or fire.

Thus, the slope must be maintained as per professional advice, especially the existing vegetation on the slope shall be kept as much as possible.

6.0 Geotechnical Hazard Statement

Given site surface/subsurface conditions and slope stability analysis above, the site is considered to be feasible for the proposed development provided that our geotechnical recommendations in this report are followed in the design and construction of the project. It is our professional opinion that the probability of landslide hazard on the site is Very Low (<1:10,000 per annum) in accordance with the hazard acceptability criteria. The land may be used safely for the use intended. Safe site use is defined as a residential building. The EGBC Landslide Assessment Assurance Statement Appendix D is attached.

7.0 Further Geotechnical Review

All engineering design recommendations presented in this report are based on the assumption that an adequate level of review will be provided during the design and construction.

Evertek requests the opportunity to review the design drawings during design and to advise on the geotechnical aspects of specifications for inclusion in design and contract documents, and the excavation base and bearing surfaces for footing foundations during construction.



8.0 Closure

This report is based on the findings at three test pit locations. Should different subsoil and groundwater conditions be encountered during construction, this office should be notified and recommendations submitted herein will be reviewed and revised as required. This report should be applied only to the presently proposed development. A contingency amount should be included in construction budgets to allow for the possibility of variations in soil conditions that may result in modification of the design and/or changes to construction procedures. Likewise, contingency plans should be developed prior to the start of construction to deal with the potential issues identified by the report.

This report has been prepared for the exclusive use of the client for the specified application to the project described in this report. The City of West Kelowna may also rely on the findings of this report. It has been prepared in accordance with generally accepted geotechnical engineering practices. No other warranty, expressed or implied, is made.

We trust that the information provided in this report meets your requirements. Should you have any questions please do not hesitate to contact this office.

Respectfully submitted,

Evertek Engineering Limited

(EGBC Permit to Practice No. 1000729)

Reviewed by:

Derek Emslie, EIT, M.A.Sc.

Derok Emplie

Junior Geotechnical Engineer

Larry Deng, M.Sc, P.Eng.

Senior Geotechnical Engineer, Principal

Attachments:

Site Photographs

Figure 1 – Site Location Plan Figure 2 – Test Pit Location Plan

Test Pit Logs

Figure 3 – Global Stability Analysis – Cross Section Locations

Figures 4 to 6 – Global Stability Analysis Results Architectural Site Plan by R-tistry Home Design.

Topographic Site Plan by Vector Geomatics Land Surveying Ltd. EGBC Landslide Assessment Assurance Statement Appendix D



ATTACHMENTS





Photo 01 Lot general view, looking east.



Photo 02 Test pit TP23-01 location, looking north.





Photo 03 Test pit TP23-01 excavated profile



Photo 04 Test pit TP23-02 excavated profile





Photo 05 Lower, east slope 28-32 degrees, looking north.



Photo 06 Upper, west slope 28-32 degrees, looking north.



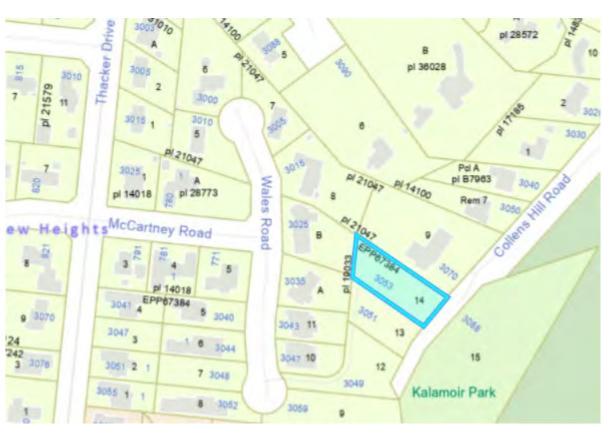
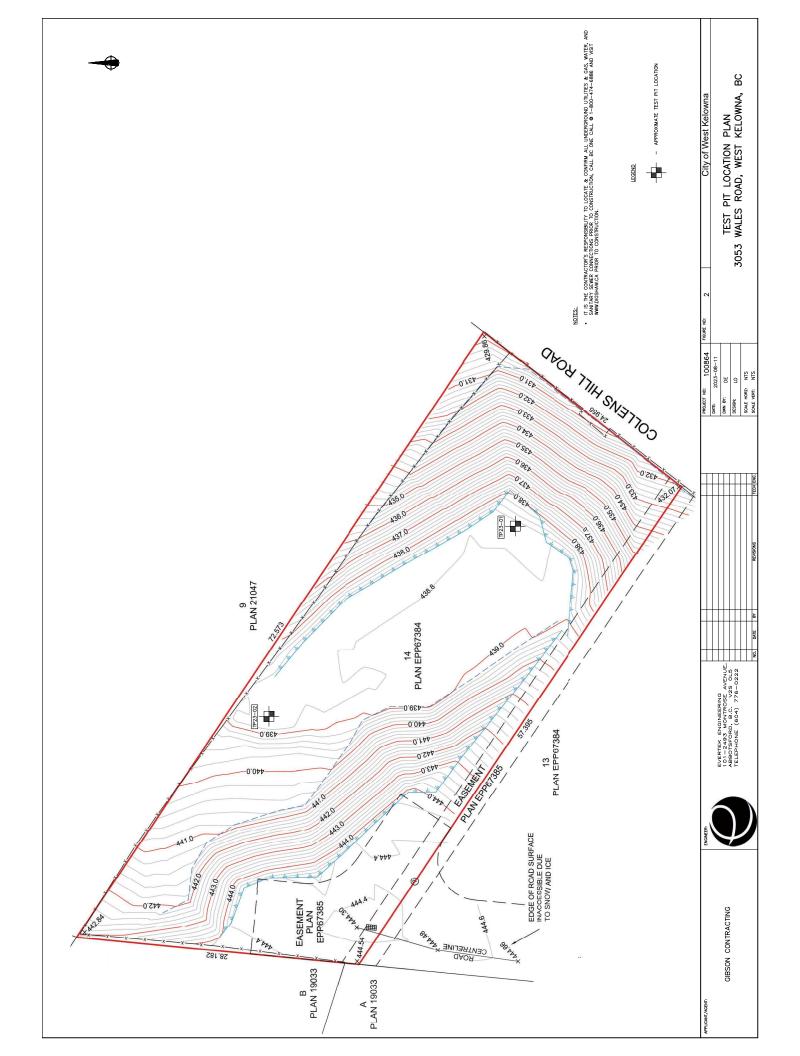


Figure 1: Site Location Plan





TEST PIT LOG TP23-01

PROJECT NUMBER: 100864
CLIENT NAME: Gibson Contracting
PROJECT: Geotechnical Assessment
SITE ADDRESS: 3053 Wales Road, West

EQUIPMENT: Mini Excavator SURFACE ELEVATION: DEPTH OF TEST PIT: 2.4 m DEPTH OF GROUNDWATER:

DATE: August 11, 2023

Kelowna, BC

COMMENTS

LOGGED BY AS

			200025		
Depth (m)	Graphic Log	Soils Description	0 Moisture (%)	DCPT Values	Depth (ft)
- - - - - -		FILL: angular blast rock fragments mixed with silty sand, with occasional rootlets, dry to damp, compact to dense, at the bottom very dense.			0.5 1 1.5 2 2.5
- -1 - - - - -					- 3 - 3.5 - 4 - 4.5 - 5 - 5.5
- - 2 - -					6.5 7 7.5
- - - -		Termination of test pit at 2.4 m below existing grade due to mechanical refusal. No groundwater was observed upon completion of test pit excavation.			8.5 9 9.5
-3 - - -					— 10 — 10.5 — 11 — 11.5 — 12
-					— 12.5 — 13



TEST PIT LOG TP23-02

PROJECT NUMBER: 100864
CLIENT NAME: Gibson Contracting
PROJECT: Geotechnical Assessment
SITE ADDRESS: 3053 Wales Road, West

SURFACE ELEVATION:
DEPTH OF TEST PIT: 1.5 m
DEPTH OF GROUNDWATER:

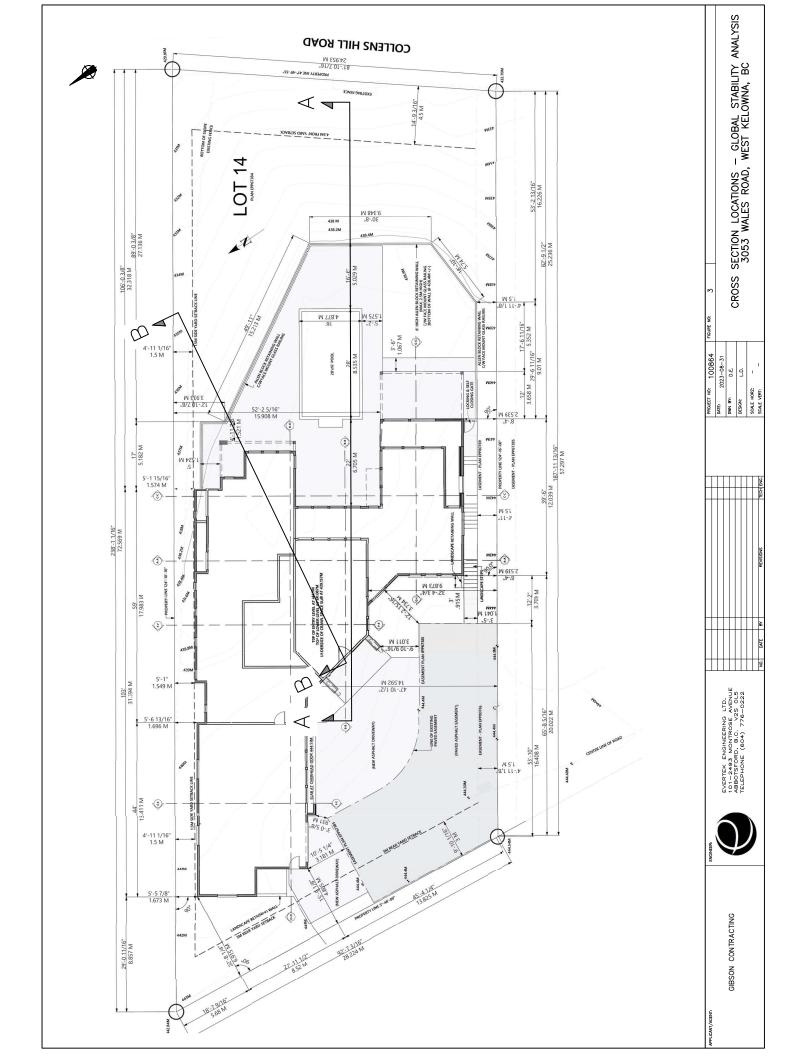
EQUIPMENT: Mini Excavator

Kelowna, BC

DATE: August 11, 2023

COMMENTS	LOGGED BY AS
OUNIMENTO	EGGGED B1 AG

	1		1		
Depth (m)	Graphic Log	Soils Description	0 Moisture (%)	DCPT Values	Depth (ft)
		FILL: angular blast rock fragments mixed with silty sand, with occasional rootlets, damp, compact.			
-		Tooliets, damp, compact.			— 0.5
-					_1
-					— 1.5
-					
					-2
-					— 2.5
-					-3
<u> </u>		CTL CAND			— 3.5
		Silty SAND, damp, compact to dense. Some grass at top of layer.			– 4
-					
-					— 4 .5
		Termination of test pit at 1.5 m below existing grade due to mechanical			5
		refusal. No groundwater was observed upon completion of test pit excavation.			- 5.5
-					-6
-					− 6.5
_ 2					_ 7
-					
-					— 7.5
-					-8
					— 8.5
-					- 9
-					— 9.5
- - 3					— 10
-					— 10.5 —
-					— 11
					— 11.5
-					— 12
-					— 12.5
					— 13
Disclaim	~=			D.	ana 2 of 2





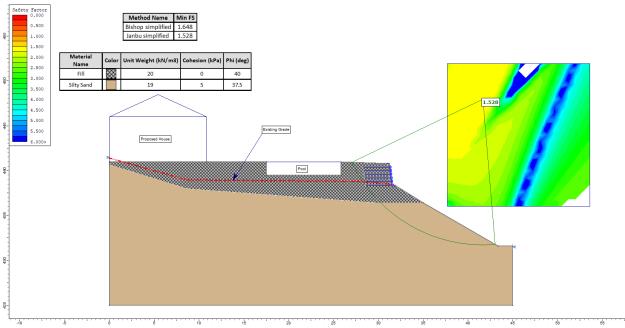


Figure 4. Rocscience Slide2D Analysis – Static Condition (Cross Section A-A)

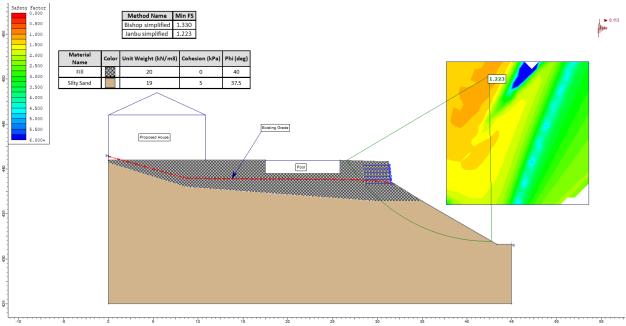


Figure 5. Rocscience Slide2D Analysis – Seismic Condition (Cross Section A-A)



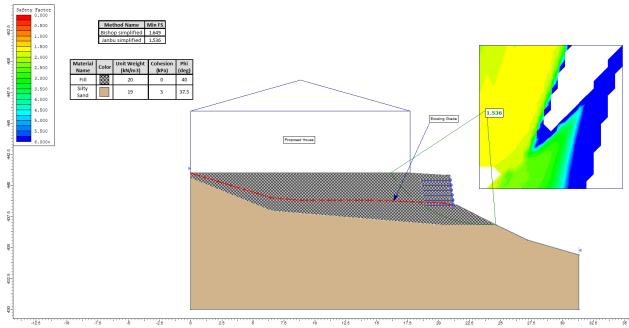


Figure 6. Rocscience Slide2D Analysis – Static Condition (Cross Section B-B)

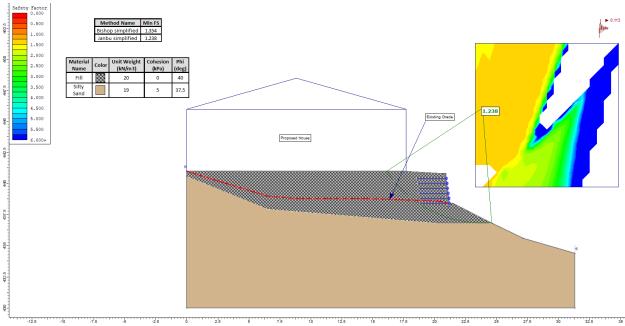
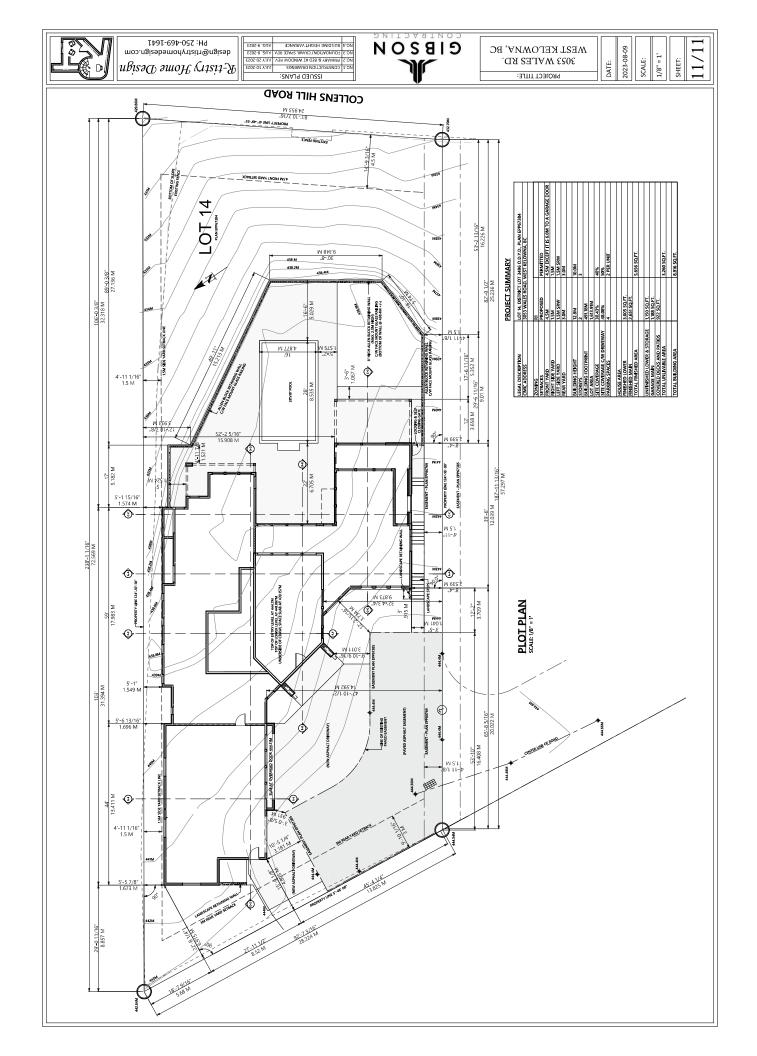
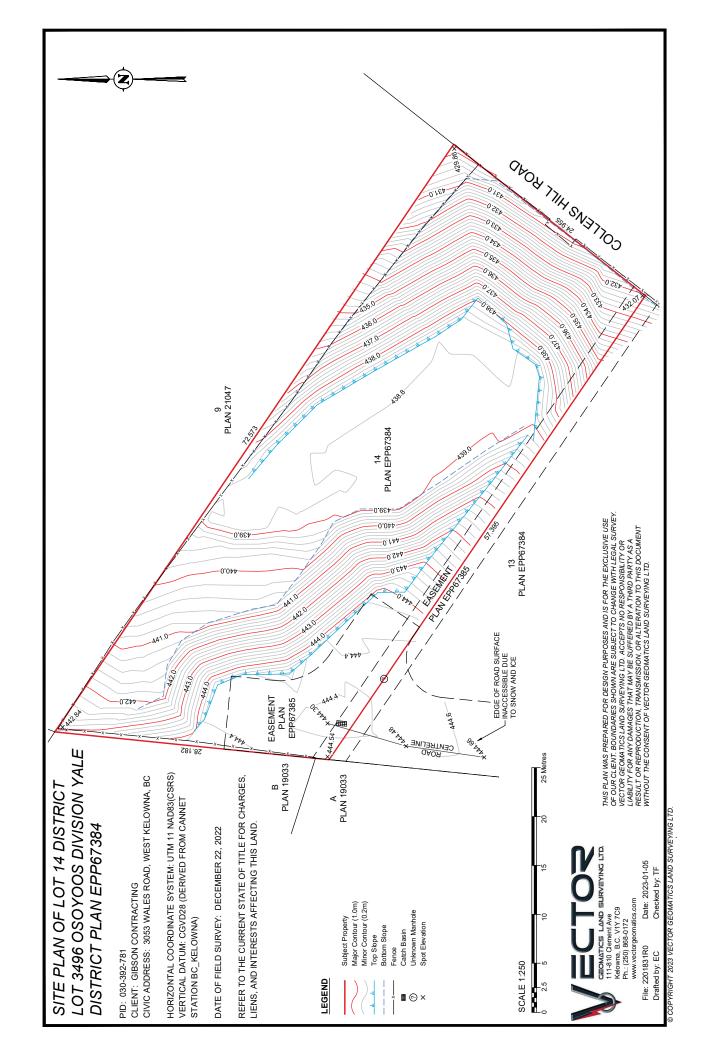


Figure 7. Rocscience Slide2D Analysis – Seismic Condition (Cross Section B-B)





LANDSLIDE ASSESSMENT ASSURANCE STATEMENT

Notes: This statement is to be read and completed in conjunction with the Engineers and Geoscientists BC *Professional Practice Guidelines – Landslide Assessments in British Columbia* ("the guidelines") and the current *BC Building Code* (*BCBC*), and is to be provided for Landslide Assessments (not floods or flood controls), particularly those produced for the purposes of the *Land Title Act*, *Community Charter*, or *Local Government Act*. Some jurisdictions (e.g., the Fraser Valley Regional District or the Cowichan Valley Regional District) have developed more comprehensive assurance statements in collaboration with Engineers and Geoscientists BC. Where those exist, the Qualified Professional is to fill out the local version only. Defined terms are capitalized; see the Defined Terms section of the guidelines for definitions.

To:	The	ne Approving Authority (or Client)		Date:		
	City of West Kelowna					
	276	60 Cam	eron Road, West Kelowna, BC V1Z 2T6			
	Juris	sdiction	name and address			
/			(OUEOK ONE)			
VVILL	reie		O (CHECK ONE):			
			and Title Act (Section 86) – Subdivision App			
			ocal Government Act (Sections 919.1 and 9	· · · · · · · · · · · · · · · · · · ·		
	Z		ommunity Charter (Section 56) – Building P	ermit		
		D. N	on-legislated assessment			
For	the fo	ollowing	property (the "Property"):			
305	3 W	ales Ro	ad, West Kelowna, BC			
		Civic a	ddress of the Property			
		•	, ,	nalified Professional and a professional engineer or professional ce requirements as outlined in the guidelines.		
	•		uthenticated, and dated, and thereby certifie the guidelines. That report must be read in	d, the attached Landslide Assessment Report on the Property in conjunction this statement.		
In pi	repar	ing that	report I have:			
[CHE	CK TO	O THE LE	FT OF APPLICABLE ITEMS]			
<u>✓</u>	1.	Collect	ed and reviewed appropriate background in	nformation		
<u>✓</u>		Reviev	ved the proposed Residential Development	or other development on the Property		
<u>√</u>	3.	Condu	cted field work on and, if required, beyond t	he Property		
✓_	4.	Report	ed on the results of the field work on and, if	required, beyond the Property		
✓_	5.	Consid	lered any changed conditions on and, if req	uired, beyond the Property		
	6.	For a L	andslide Hazard analysis or Landslide Risk	analysis, I have:		
	<u>√</u>	-	reviewed and characterized, if appropriate	any Landslide that may affect the Property		
	√	6.2	estimated the Landslide Hazard			
	<u>√</u>	6.3	•	ements at Risk on and, if required, beyond the Property		
	<u>✓</u>	6.4	estimated the potential Consequences to t			
	7.		the Approving Authority has adopted a Lev			
		7.1	compared the Level of Landslide Safety ac investigation	lopted by the Approving Authority with the findings of my		
		7.2	made a finding on the Level of Landslide S	afety on the Property based on the comparison		
		7.3	made recommendations to reduce Landslie	de Hazards and/or Landslide Risks		

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LANDSLIDE ASSESSMENT ASSURANCE STATEMENT

	✓	Where the Approving Authority has not adopted a Level of Landslide Safety, or where the Landslide Assessment is not produced in response to a legislated requirement, I have: 8.1 described the method of Landslide Hazard analysis or Landslide Risk analysis used 8.2 referred to an appropriate and identified provincial, national, or international guideline for Level of Landslide
	<u>√</u> <u>√</u>	Safety 8.3 compared those guidelines (per item 8.2) with the findings of my investigation 8.4 made a finding on the Level of Landslide Safety on the Property based on the comparison 8.5 made recommendations to reduce Landslide Hazards and/or Landslide Risks
	9.	Reported on the requirements for future inspections of the Property and recommended who should conduct those inspections
Bas	ed on	n my comparison between:
[CHE	ECK OI	NE]
\square		findings from the investigation and the adopted Level of Landslide Safety (item 7.2 above) appropriate and identified provincial, national, or international guideline for Level of Landslide Safety (item 8.4 above)
		e Landslide Assessment is not produced in response to a legislated requirement, I hereby give my assurance that, the conditions¹ contained in the attached Landslide Assessment Report:
A.	SUE	BDIVISION APPROVAL
		subdivision approval, as required by the Land Title Act (Section 86), "the land may be used safely for the use intended" [CK ONE]
		with one or more recommended additional registered Covenants without an additional registered Covenant(s)
В.	DEV	/ELOPMENT PERMIT
	gove	a <u>development permit</u> , as required by the <i>Local Government Act</i> (Sections 488 and 491), my report will "assist the local ernment in determining what conditions or requirements it will impose under subsection (2) of [Section 491]" ECK ONE]
		with one or more recommended additional registered Covenants without an additional registered Covenant(s)
C.	BUII	LDING PERMIT
V	inter	a <u>building permit</u> , as required by the <i>Community Charter</i> (Section 56), "the land may be used safely for the use nded"
	-	CCK ONE]
	□ Z	with one or more recommended additional registered Covenants without any additional registered Covenant(s)

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When seismic slope stability assessments are involved, Level of Landslide Safety is considered to be a "life safety" criteria, as described in Commentary JJJ of the *National Building Code of Canada (NBC) 2015*, Structural Commentaries (User's Guide – NBC 2015: part 4 of division B). This states:

[&]quot;The primary objective of seismic design is to provide an acceptable level of safety for building occupants and the general public as the building responds to strong ground motion; in other words, to minimize loss of life. This implies that, although there will likely be extensive structural and non-structural damage, during the DGM (design ground motion), there is a reasonable degree of confidence that the building will not collapse, nor will its attachments break off and fall on people near the building. This performance level is termed 'extensive damage' because, although the structure may be heavily damaged and may have lost a substantial amount of its initial strength and stiffness, it retains some margin of resistance against collapse."

LANDSLIDE ASSESSMENT ASSURANCE STATEMENT

Larry H Deng	August 31, 2023
Name (print)	Date
101-2493 Montrose Avenue, Abbotsford, BC	V2S 0L5
Address	_
604-776-0222	- N. DENG
Telephone	- #30†37 PHTINE
larry.deng@evertekengineering.com	2023-08-31
Email	(Affix PROFESSIONAL SEAL and signature here)
The Qualified Professional, as a registrant on the	e roster of a registrant firm, must complete the following:
EVERTEK ENGINED I am a member of the firm	ERING LTD.
	(Print name of firm)
1000729 with Permit to Practice Number	
	(Print permit to practice number)
and I sign this letter on behalf of the firm.	

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